## When Buttressing Matters: a sensitivity study

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#### **MOTIVATION**

- Ice shelves can buttress their ice streams
- Weaker ice shelves will buttress less
- Thinning and upstream migration of the grounding line may result



### **GOAL & APPROACH**

Goal : Assess the sensitivity of stream/shelf systems to a change in buttressing

Approach: Use a simple model to examine how an initially steady-state system responds to a loss of buttressing

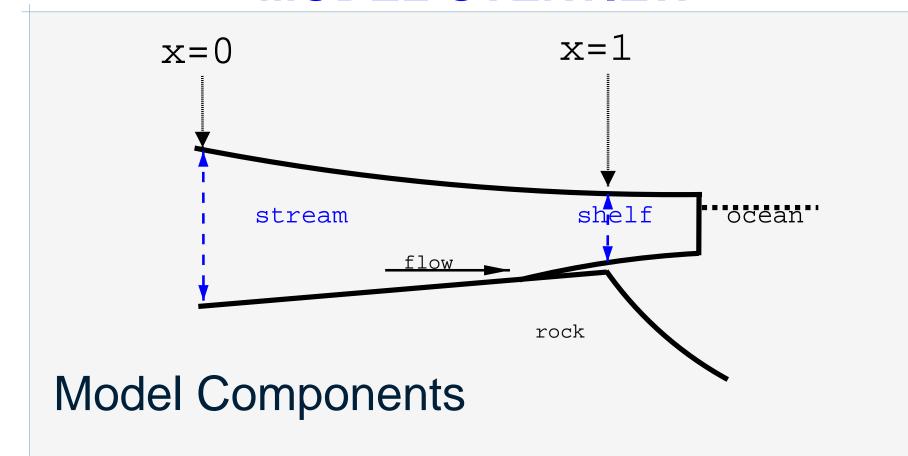


#### **SNEAK PREVIEW**

- Ice shelves do matter, at least for "PIG-like" systems
- We have a nice tool ideal for reconnassance style studies



# **MODEL OVERVIEW**



- diagnostic momentum balance
- prognostic mass balance



## **MOMENTUM BALANCE**

- 1-d flowline, nondimensionalized, FEM treatment
- derived similarly to the plan-view eqn's of MacAyeal (1989)
- treats basal drag and lateral drag as boundary layer phenom.
- includes long. dev. stress
- appropriate for thin, channelized, free-surface, 'plug' flow
- buttressing applied as a boundary condition



## **MOMENTUM BALANCE cont'd**

$$\frac{\partial}{\partial x} \left( 2h\nu \frac{\partial u}{\partial x} - \frac{A}{2}h^2 \right) = G_s h u^{\frac{1}{n}} + \begin{cases} A\beta h + G_b u^{\frac{1}{m}} & h > h_f \\ -\frac{A}{2} \frac{1}{r_{sw}} \partial_x h^2 & h \leq h_f \end{cases}$$

 $stretching-press. grad. = side drag + \begin{cases} basal drag & grounded \\ ocean press. floating \end{cases}$ 

where x is the along-flow coordinate, h is thickness, u is velocity, n and m are the ice and basal flow-law exponents,  $r_{sw} = \rho_{sw}/\rho_i$  is nondim. density of seawater,  $\beta$  is the bed slope, and  $\nu \equiv \left|\frac{\partial u}{\partial x}\right|^{\frac{1-n}{n}}$  is the strain-rate dependent viscosity.

- *A* is a measure of the importance of ice thickness gradients
- G<sub>b</sub> measures the importance of basal drag
- ullet  $G_s$  measures the importance of side drag



### **MOMENTUM BALANCE cont'd**

#### Boundary conditions:

- Upstream (x = 0) boundary condition  $u(0, t) = u_0$
- Downstream, or terminal, (x = 1) boundary condition

$$\left[2h\nu\frac{\partial u}{\partial x} - \frac{A}{2}h^2\right]_{x=1} = -f\frac{A}{2}h(1)^2 - (1-f)\,r_{sw}\frac{A}{2}z_b(1)^2$$

f is the **buttressing parameter**, such that

- $\star f = 1 \leadsto$  fully buttressed condition
- $\star$   $f = 0 \sim$  freely-spreading condition = unbuttressed



## **MASS BALANCE**

- 1-d, time-dependent, non-dimensional
- derived from depth-integrated continuity
- neglects accumulation & lateral variations in thickness

$$\frac{\partial h}{\partial t} = -\frac{\partial}{\partial x} (uh)$$

thickening rate = flux convergence

#### Boundary condition:

• fixed upstream thickness,  $h(0,t) = h_0$ 



### **EXPERIMENTAL APPROACH**

- Start with a system which is at steady-state with 50% buttressing (f=0.5)
- Remove buttressing (f=0) and watch the system adjust

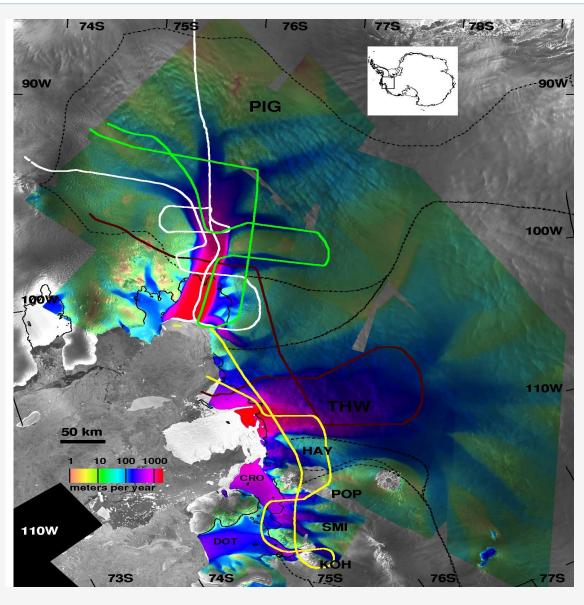


#### **EXPERIMENTS**

- Performed a reference experiment using "PIG-like" numbers
- Many sensitivity experiments were conducted (e.g., 20% incr. in G<sub>s</sub>, or 20% decr. A)



# **PIG GEOMETRY**



From Rignot et al., Ann. Glaciol., 39, in press



# **PIG-LIKE SCALES**

Scale, constant or parameter	Value
H	1 km
$L_x$	100 km
$L_y$	20 km
U	$7.6  imes 10^{-5}~\mathrm{ms}^{-1} pprox 2.4~\mathrm{km/year}$
$B_i$	$2  imes 10^8~{ m Pa~s}^{1/3}$
$ au_b$	0.73 bar
$ au_y$	5.5 bar
$T = L_x/U$	$1.3  imes 10^9 \  extsf{s} pprox 41 \  extsf{years}$

$$A \equiv \frac{\rho_i g H}{B_i \left(\frac{U}{L_x}\right)^{\frac{1}{n}}} = 50 \quad G_b \equiv \frac{\tau_b L_x}{H B_i \left(\frac{U}{L_x}\right)^{\frac{1}{n}}} = 40 \quad G_s \equiv \frac{\tau_y L_x}{L_y B_i \left(\frac{U}{L_x}\right)^{\frac{1}{n}}} = 15$$

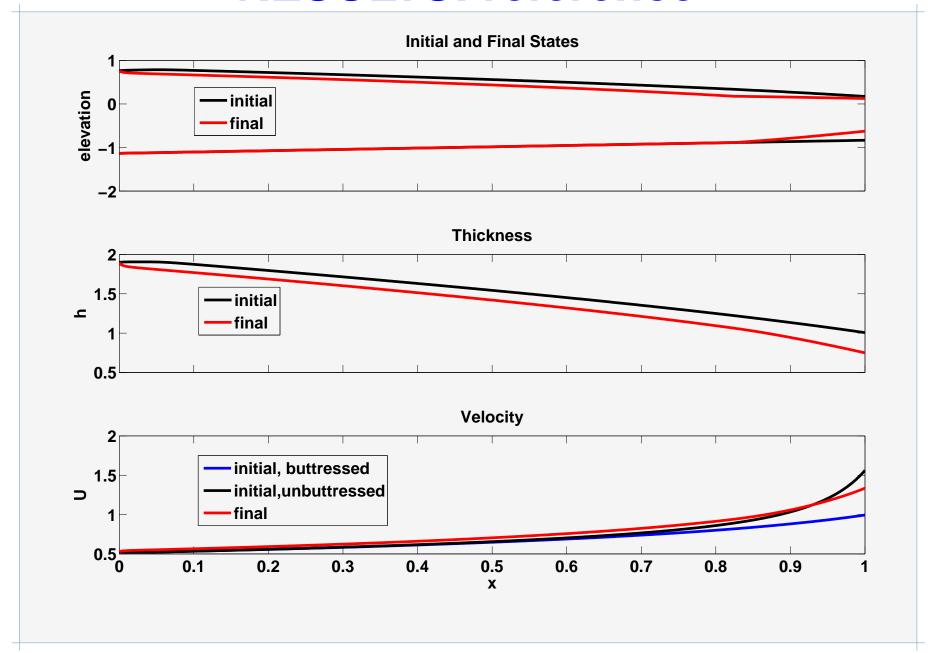


# **EXPERIMENTS**

experiment	$G_s$	$\beta$	$G_b$	A	$h_0$	$u_0$
reference	15	0.3	40	50	1.9	0.53
$+G_s$	18					
<b>-</b> β		0.24				
$+G_b$			48			
<b>+</b> A				60		
<b>-</b> A				40		
$+h_0$					2.3	
$+u_0$						0.63

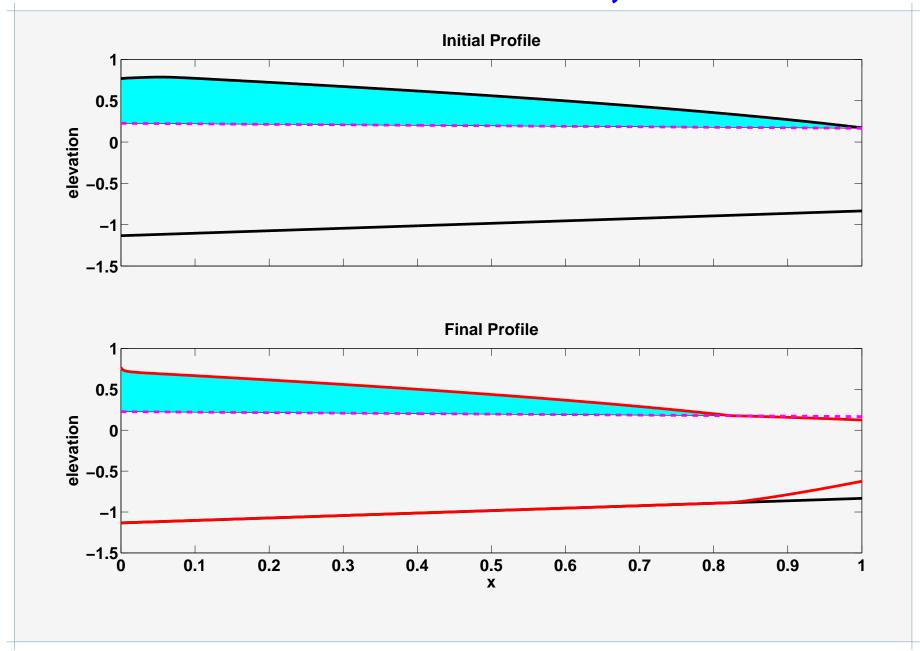


# **RESULTS:** reference



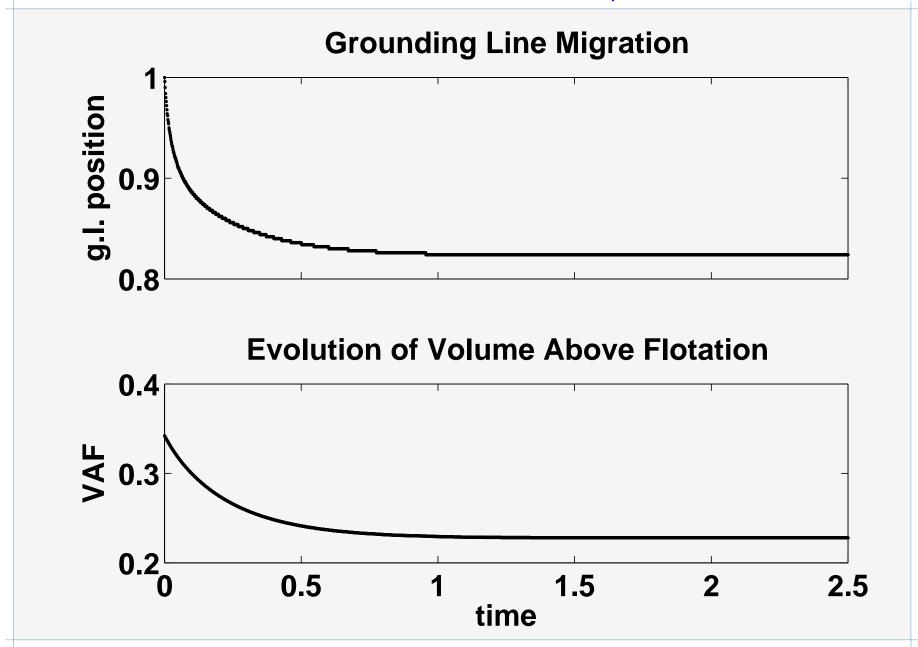


# **RESULTS:** reference, cont'd





# **RESULTS:** reference, cont'd





# **SENSITIVITY RESULTS**

experiment	g.l. retreat	init'l VAF	final VAF	VAF loss
				(% of init'l)
reference	0.18	0.34	0.23	0.11 (33%)
+20% in $G_s$	0.14	0.37	0.27	0.10 (27%)
-20% in $eta$	0.17	0.35	0.24	0.11 (32%)
+20% in $G_b$	0.17	0.38	0.26	0.12 (32%)
+20% in A	0.22	0.21	0.14	0.11 (43%)
-20% in $\it A$	0.08	0.43	0.35	0.09 (20%)
+20% in $h_0$	0.18	0.34	0.23	0.12 (34%)
+20% in $u_0$	0.14	0.39	0.28	0.11 (28%)



#### **CONCLUSIONS**

- Loss of buttressing results in notable g.l. retreat and VAF loss (18 km &  $\sim$ 300 km<sup>3</sup>, respectively, using PIG scales)
- Thinning extends far upstream
- † buttressing sensitivity for ↓ side drag and †
   driving stress († basal drag)
- Siple Coast ice streams may be vulnerable
- Results are likely conservative
  - \* fixed upstream thickness
  - \* no sub-ice-shelf melting



#### **FUTURE WORK**

- Adaptive meshing → better efficiency
- Include dynamic accumulation/melting
- Free the upstream boundary
- Perform new, "improved", PIG-like experiments
- Perform Siple experiments

